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Welding — Basic welded joint details in steel — Part 1: Pressurized components

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Зварювання. Зварні з'єднання сталевих елементів Частина 1. Зварні з'єднання конструкційних елементів, що працюють під тиском

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This European Standard was approved by CEN on 28 November 2009.

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Foreword

This document (EN 1708-1:2010) has been prepared by Technical Committee CEN/TC 121 "Welding", the secretariat of which is held by DIN.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by July 2010, and conflicting national standards shall be withdrawn at the latest by July 2010.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN [and/or CENELEC] shall not be held responsible for identifying any or all such patent rights.

This document supersedes EN 1708-1:1999.

EN 1708, Welding — Basic weld joint details in steel, consists of the following parts:

- Part 1: Pressurized components
- Part 2: Non internal pressurized components

According to the CEN/CENELEC Internal Regulations, the national standards organizations of the following countries are bound to implement this European Standard: Austria, Belgium, Bulgaria, Croatia, Cyprus, Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, Netherlands, Norway, Poland, Portugal, Romania, Slovakia, Slovenia, Spain, Sweden, Switzerland and the United Kingdom.

1 Scope

The purpose of this European Standard is to exemplify commonly accepted welded connections in pressure systems. It does not promote the standardization of connections that may be regarded as mandatory or restrict development in any way. Stress analysis rules should be considered if necessary.

This standard contains examples of connections welded by:

- Manual metal-arc welding with covered electrode (111);
- Submerged arc welding (12);
- Gas shielded metal arc welding (13);
- Tungsten inert gas arc welding; TIG-welding (14);
- Plasma arc welding (15)

processes (process numbers according to EN ISO 4063) in steel pressure systems. Other processes by agreement.

This standard covers welded joint details in steel, but can be applied to other metallic materials. In such cases the shape and dimensions of the weld should be checked.

The estimation of the suitability of welded connections for special service conditions, for example corrosion and fatigue are not specially considered.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

EN ISO 4063, Welding and allied processes — Nomenclature of processes and reference numbers (ISO 4063:2009)

EN ISO 5817, Welding — Fusion-welded joints in steel, nickel, titanium and their alloys (beam welding excluded) — Quality levels for imperfections (ISO 5817:2003, corrected version:2005, including Technical Corrigendum 1:2006)

EN ISO 9692-1:2003, Welding and allied processes — Recommendations for joint preparation — Part 1: Manual metal-arc welding, gas-shielded metal-arc welding, gas welding, TIG welding and beam welding of steels (ISO 9692-1:2003)

EN ISO 9692-2:1998, Welding and allied processes — Joint preparation — Part 2: Submerged arc welding of steels (ISO 9692-2:1998)

3 Requirements

3.1 Selection of detail

Connections are not considered to be equally suitable for all service conditions, nor is the order in which they are shown indicative of their relative characteristics. In selecting the appropriate detail to use from the several

alternatives shown for each type of connection, consideration shall be given to existing fabrication and service conditions that pertain.

3.2 Joint preparation (geometry and size)

3.2.1 General

The limitations quoted in weld profiles and sizes are based on commonly accepted practice, but they may be subjected to modifications if required by special welding techniques or design conditions, which should be included in the design documents and in the welding procedure specifications (WPS).

3.2.2 Joint preparation geometry

Examples of recommended joint preparation geometry (e.g. bevel angles, root radius, presence of backing strips, root faces) are referred to EN ISO 9692-1 when applicable and to EN ISO 9692-2 relative to submerged arc welding process. Missing dimensions of preparations are in accordance with EN ISO 9692-1.

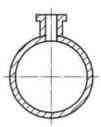
In case where full penetration butt joints are indicated, it is intended that they shall be back chipped or gouged and back welded, or alternatively that the welding procedure shall be such as to ensure sound, effective root penetration.

For relevant difference of thickness (generally a difference of about 3 mm (see Table 1, no. 1.1.1 to 1.1.6) could be considered relevant; in any case the thickness of material shall be taken into account, as well as the shape of the joint) of parts to be butt welded, the thickest element shall be shaped with a slope of 1:5 up to 1:2. Smoother transition of wall thickness is applicable in severe service conditions.

3.2.3 Weld sizes

The thickness of welds (in particular of fillet welds), which are not determined by their profile, are based on the assumption that the connection need not be stronger than the connected parts.

3.3 Presentation





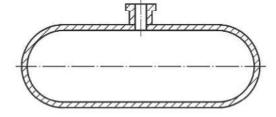


Figure 2 — Longitudinal section

The drawings of the nozzle and branch connections (see Tables 2 and 3) show a transversal section of the connection (see Figure 1) and a longitudinal section of the connection (see Figure 2).

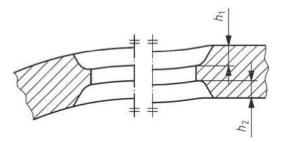
3.4 Removal of internal sharp edges in branch bores

It will be noted that the internal edges on the bores of branches are shown partially radiused (for example see Table 2, no. 2.1.6) because a stress concentration occurs at this point. The rounding of the edges is recommended when the branch connection is subjected to severe service conditions like fatigue, creep and stress corrosion.

3.5 Preparation of holes in shell for set-through branches

In case of set-in and set-through branches (according to Table 2, no. 2.2 and no. 2.3) holes in the shell may be cut and profiled in two ways as follows:

— The depth of the grooves h_1 and h_2 may be constant around the hole as shown in Figure 3.



Key h_1, h_2 depth of the grooves

Figure 3 — Preparation of holes in the shell

— The roots of the joint preparations may be in one plane, as for example when they are machine drilled, in which case the depths of the grooves will vary around the hole as shown in Figure 4.

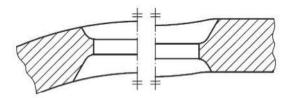


Figure 4 — Preparation of holes in the shell

3.6 Welds for smooth transition

In some cases it is convenient to foresee a fillet weld providing smooth geometric transition from the surface of one welded part to the surface of the other one, e.g. from branch to shell. Its purpose is to soften the notch effect in the branch-shell edge and therefore the throat thickness is not presented on the figure concerned.

3.7 Oblique and tangential branches

The welded connections are contained in Tables 1 to 13. Regarding branches, the oblique and tangential ones are not specially considered as their preparation is similar to that reported on Tables 2 and 3 for radial branches. Only some significant cases are therefore considered (see Table 2, no. 2.2).

NOTE 1 The welds are only blackened in the following tables when the figures do not give information about the dimension of the values for the preparation.

NOTE 2 It is not intended that the values of the dimension given in the tables should be measured precisely but rather the general philosophy should be applied.

Table 1 — Butt joints of different thickness

1.1.4	1.1.3	1.1.2	1.1.1		no.
t_1 t_2 Q	t_1	<i>t</i> ₁	$\frac{t_1}{e}$	1.1 Butt jo	Figure
α ≤ 30°	α ≤ 30° t₁ < t₂	$\alpha \le 30^{\circ}$ $t_1 < t_2$	$\alpha \le 30^{\circ}$ $t_1 < t_2$	1.1 Butt joints in plates of different thickness	Application/ condition
see 1.1.1	for ultrasonic test $h > 3$ t_1 , but min. 20 mm for radiographic test $h \ge t_1$		In case of severe service conditions, the design shall be in accordance with Figures 1.1.2 and 1.1.3. $e \le 0,1 t_1$ max. 2 mm (for one side welding)	hickness	Note
2.5.1	1.5, 2.3 and 2.5.2	1.5, 2.3 and 2.5.2	1.5 and 2.3		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

1.1.6	1.1.5	no.
	t_1	Figure
α ≤ 30°	α. ≤ 30°	Application/ condition
for ultrasonic test $h > 3$ t_1 , but min. 20 mm for radiographic test $h \ge t_1$		Note
2.5.1	2.5.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 1 (continued)

no.	1.1.7							
Figure	h ₂	2	h ₁					
Application/ condition	longitudinal weld:	$h_1 \le 0,15 t_1$; maximum 3 mm	$h_2 \leq 0,3 t_1$; maximum 6 mm	$t_2 - t_1 \le 0,3 t_1$; maximum 6 mm	circumferential weld:	$h_1 \le 0,2 t_1$; maximum 5 mm	$h_2 \le 0.4 t_1$; maximum 10 mm	$t_2 - t_1 \le 0.4 t_1$; maximum 10 mm
Note								
Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998								

Table 1 (continued)

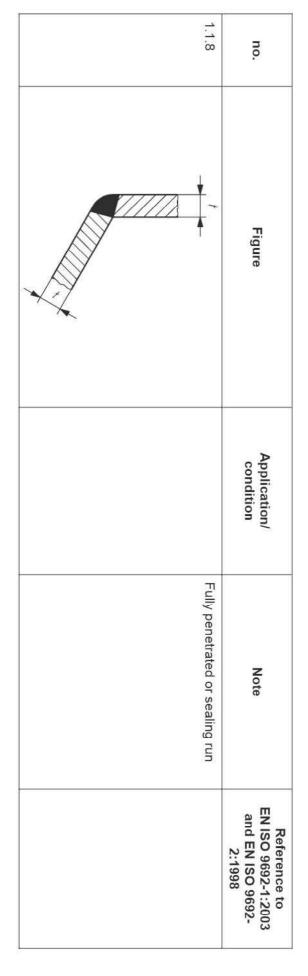


Table 2 — Branches without compensation rings

2.1.2	2.1.1	If the shell is		no.	
		2.1 Set-on branches (for special branch connections see 13.2) If the shell is stressed in direction of the thickness, it should be examined for laminations before setting on the branch.	These connections include the provision of compensation by thickening of the branch and/or shell.	Figure	Idbid 7 — E
$45^\circ \le \alpha_1 \le 60^\circ$ $30^\circ \le \alpha_2 \le 45^\circ$	$t_1 < 0.5 t_2$ $45^{\circ} \le \alpha \le 60^{\circ}$	2.1 Set-on branches (for special branch connections see 13.2) ness, it should be examined for laminations before setting on the	ision of compensation by thic	Application/ condition	lable z — Bialiciles Willout compensation
These details are recommended only where the bore of the branch is readily accessible for welding. The joint should be back-gouged from the side most accessible and suitable for this purpose generally from the outside.		ections see 13.2) re setting on the branch.	kening of the branch and/or shell.	Note	anon inigs
2.9.1, 2.9.2 or 2.11	1.9.1 or 1.11 one side welding			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998	

Table 2 (continued)

2.1.4	2.1.3	no.
		Figure
no gap $c \ge 1,5 \text{ mm}$ $r \ge 5 \text{ mm}$ $\alpha = 30^{\circ}$	$\alpha_1 = 30^\circ$ $\alpha_2 = 45^\circ$	Application/ condition
 Joints generally used for small branch to shell diameter ratios. Diameter d to be bored out after welding to remove the weld root, in order to ensure sound weld. 	See 2.1.2	Note
1.9.1 or 1.11 one side welding		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.1.6	2.1.5	no.
		Figure
For branches up to approximately 100 mm bore. 1 mm $\le b \le 3$ mm $h \le 5$ mm $c = 1$ mm $c = 1$ mm $r = 7$ mm $\alpha_1 \le 45^\circ$ $\alpha_2 \le 45^\circ$	10 mm $\le l \le 15$ mm $h \ge 3$ mm 30° $\le \alpha \le 45$ °	Application/ condition
Generally used for the attachment of branches to thick-walled shells.	Joints generally used for small branch to shell diameter ratios.	Note
	1.11 one side welding	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.1.9	2.1.8	2.1.7	no.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} D \\ D \\ D \\ D \\ D \\ D \\ 1 \\ D \\$	h	Figure
$A = 5 \text{ mm}$ $B = 5 \text{ mm}$ $C = 5 \text{ mm}$ $E = t$ $F = 1,5 \text{ mm}$ $G = 0,5 \text{ mm}$ $\alpha = 30^{\circ}$ $1 = \text{Profile to meet}$ design requirements	$r = 3 \text{ mm}$ $E = 6 \text{ mm}$ $F = 1,5 \text{ mm}$ $\alpha = 30^{\circ}$ $\alpha = 30^{$	<i>h</i> ≤ 3 mm	Application/ condition
For tubes or nozzles up to and including 150 mm bore and wall thickness t over 6 mm and up to and including 13 mm.	For tubes or nozzles up to approximately 100 mm bore and 6 mm wall thickness t.	The sizes of the fillet welds should be based on the loads transmitted, paying due attention to other fabrication and service requirements.	Note
			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.1.11	2.1.10	no.
	Dimensions in millimetres $\frac{D}{A} = \frac{1}{A}$ $\frac{1}{A}$	Figure
F = 2 mm G = 1,5/2,0 mm T = 16 mm max. $45^{\circ} \le \alpha \le 60^{\circ}$	A = 30 mm B = 1,5 mm $H \ge 3 \text{ mm}$ $M \ge 10 \text{ mm}$ N = 5 mm $W \ge 2 \text{ mm}$ r = 6 mm $\alpha = 30^{\circ}$ 1 = Fin material 2 = Weld access hole (filled after welding tube to header)	Application/ condition
For all tube and nozzle sizes.	Tube panel connections only applicable to tubes up to 100 mm bore and 6 mm wall thickness t.	Note
		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.2.2	2.2.1	As a general for the purpos	no.
		2.2 Set-in branches (for special branch connection As a general recommendation all set-in branches should be welded on the inside of the shell as stort the purpose, otherwise preference should be given to set-on branch connections as shown e.g.	Figure
$3 \text{ mm} \le a = 0.5 t_1$ $a_1 < 0.7 t_1$ $b \le 1 \text{ mm}$	$a = 0.5 t_1$ $h = t_1$ $r \ge 8 \text{ mm}$ $b \le 1 \text{ mm}$ $10^\circ \le \alpha \le 20^\circ$	Set-in branches (for special branch connection see 13.2) should be welded on the inside of the shell as shown e.g. in ven to set-on branch connections as shown e.g. in Figure 2	Application/ condition
For partial penetration welded connection. Limited application: — Internal diameter of shell ≤ 200 mm; wall thickness of branch t ₁ ≤ 5 mm.	For partial penetration welded connection. Generally used when t_1 is less than $t_2/2$. For smaller diameter branches attention is drawn to the details shown in Table 3 which may provide a preferable solution.	ection see 13.2) as shown e.g. in Figures 2.2.1 and 2.2.2 if they are accessible n e.g. in Figure 2.1.1.	Note
3.1.1 and 3.1.2	1.11 and 3.1.1	2.2.2 if they are accessible	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.2.4	2.2,3	no.
		Figure
$3 \text{ mm} \le a = 0.5 t_1$ $a_1 \le 0.7 t_1$ $b \le 1 \text{ mm}$	$a \ge 5 \text{ mm}$ $a_1 \le 0,7 t_1$ $b \le 1 \text{ mm}$ $10^\circ \le \alpha \le 20^\circ$ $r \ge 8 \text{ mm}$	Application/ condition
For full penetration welded connection.	For partial penetration welded connection.	Note
3.1.2 and 1.11	3.1.2 and 1.11	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.2.7	2.2.6	2.2.5	no.
		$\geq h_2$ h_2 h_2 h_3 h_4	Figure
$t_2 \le 3 t_1$ $30^\circ \le \alpha \le 45^\circ$ $2 \text{ mm} \le b \le 3 \text{ mm}$ $2 \text{ mm} \le c \le 4 \text{ mm}$	$t_1 \ge 3 \text{ mm}$ $t_2 \le 3 t_1$ $40^\circ \le \alpha \le 60^\circ$	$h_1 = 0,6 t_1$ $h_2 = t_1$ $b \le 1 \text{ mm}$ $r \ge 8 \text{ mm}$	Application/ condition
For full penetration welded connection.	For full penetration welded connection. For joints which are accessible from one side only.	For partial penetration welded connection.	Note
2.9.1, 2.9.2 and 2.11	1.9.1 and 1.11	2.11	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.2.8	no.
	Figure
$45^{\circ} \le \alpha \le 60^{\circ}$ $2 \text{ mm} \le b \le 3 \text{ mm}$ $2 \text{ mm} \le c \le 4 \text{ mm}$	Application/ condition
For full penetration welded connection.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

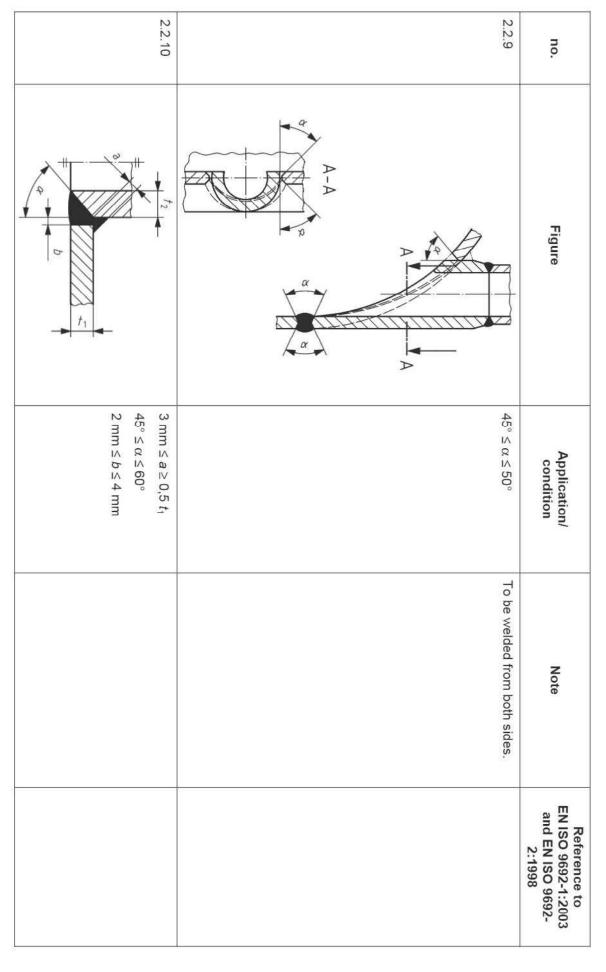


Table 2 (continued)

2.3.2	2.3.1		no.
			Figure
$h = 0.6 t_1$ $m \ge t_1$	$a = 0.5 t_1$ $b \le 1 \text{ mm}$	2.3 Set-through branch	Application/ condition
For partial penetration welded connection.	Generally used when t_1 is less than $t_2/2$.		Note
2.11	4.1		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 2 (continued)

2.5.1			2.4.1		2.3.3	no.
###	2	# #	#	2.4 Extruded branch cor		Figure
1 conventional butt joint	2.5 Butt welded branches		$m \ge t_1$ 1 conventional butt joint	Extruded branch connections (for special branch connections see 13.2)	m≥t,	Application/ condition
		Example of application: Surface coating, e.g. internal rubber lining.	Conventional butt joint will be used to weld the branch connection to the shell, and may not necessarily have the form shown.	h connections see 13.2)	For full penetration welded connection.	Note
2.5.1, 2.5.2			1.5		2.9.1 and 2.11	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 3 — Branches with compensation rings

no.
Figure
Application/ condition
Note
Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Compensatio exceed the th	Compensation rings should be fitted to the shell and vent holes should be provided in them. The thickness of the compensation ring should preferably not exceed the thickness of the shell.	es should be provided in them.	The thickness of the compensation	and EN ISO 9692- 2:1998 ring should preferably i
		3.1 Set-on branches		
3.1.1	$\pm \pm \frac{t_1}{2}$	$5 \text{ mm} \le a = 0,5 t_3,$ $b \ge 7 \text{ mm}$		
		1 for shell to branch joints, see Table 2		

Table 3 (continued)

no.
Figure
Application/ condition
Note
Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

3.2 Set-in branches

Wider gaps increase the tendency to spontaneous cracking during welding, particularly as the thickness of the parts joined increases Gap between branch and shell. It is recommended that the gap between the branch and the shell, also the compensation ring, should not exceed 3 mm.

Internal compensation ring. Set-in branches with a single compensation ring has been shown with the ring on the outside of the shell, which is the normal case. Similar connections may be used for the attachment of internal compensation ring in the formed end of pressure vessel and in spherical vessel.

						2 1	b ₁	7/			7 / Z	b_2		▼	<i>t</i> ,	3.2.1	case. Offinial compensational be used for the attachment of internal compensationing in the re-
												β ≥ 20°	30° ≤ α ≤ 45°		6 \ 7 mm	$5 \text{ mm} \le a = 0.5 t_3$	of lifeting compensation in g
												Table 2 in Figure 2.2.7	For shell to branch joints, see	preferred to compensation rings.	with big wall thickness is	Compensation of the branches 2.9.1, 2.11 and 1.10	מוכי וסוווכם כוום סו מוכישמוב עכשכו מום ווי שמוכיוכם עכשכו.
$a = 0,7 t_3$ $2 \text{ mm} \le b_1 \le 4 \text{ mm}$ $b_2 \ge 7 \text{ mm}$ $\beta \ge 20^\circ$	$a = 0,7 t_3$ 2 mm $\leq b_1 \leq 4$ mm $b_2 \geq 7$ mm	$a = 0.7 t_3$ 2 mm $\le b_1 \le 4$ mm	$a = 0,7 t_3$	2002	t ₃ < t ₂	$h > 0.7 t_3$	$a = 0.5 t_3$	α = 60°	reinforcements.	thickness shall be	her \	Reinforcements by	calculation.	shall	The reinforcements	2.9.1, 2.11 and 1.10	in opticitical vessei.

Table 4 — Sockets and couplings

4.1.3	4.1.2	4.1.1		no.
			4	Figure
m = 1,5 mm		m = 1,5 mm	4.1 Sockets and couplings	Application/ condition
see 4.1.1 Not suitable when crevice corrosion is expected.	see 4.1.1	Small couplings in 4.1.1 to 4.1.3 inclusive may be attached to shells by the connections and (with the exception of 4.1.3) by any other appropriate joint shown in Figures 2.3.1 to 2.5.1. Applications especially for attachments, e.g. temperature and pressure sensors. Not suitable when crevice corrosion is expected.		Note
3.1.2 and 1.9.1	4.1.3	3.1.1 and 4.1.3		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 4 (continued)

4.1.4	no.
	Figure
m = 1,5 mm	Application/ condition
Applications especially for attachments, e.g. temperature and pressure sensors. Not suitable when crevice corrosion is expected.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 5 — Flanges

5.1.2	5.1.1.1	Due to d The clea In the ca	no.
		Due to distortion it may be necessary to machine the flange-face after welding. The clearance between the bore of the flange and the inner diameter of the branch shall not exceed 2 mm. In the case of thick set-on flanges a radial vent hole through the flange may be useful. 5.1 Flanges (t is the tube thickness)	Figure
1 conventional butt weld	After machining flange to final thickness. $h_1 \ge 0.7 t$ $h_2 \ge 0.7 t$	re after welding. Imeter of the branch shall not excess flange may be useful. Flanges (t is the tube thickness)	Application/ condition
Welding neck flange. Refer to Table 1 from 1.1.1 to 1.1.3	Face and back welded flange. For partial penetration welded connection.	exceed 2 mm.	Note
1.5 or 1.3	1.11 and 2.11		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 5 (continued)

5.1.5	5.1.4	5.1.3	no.
1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0			Figure
$h_1 \ge 0.7 t$ $h_2 \ge 0.7 t$ $45^\circ \le \alpha_1 \le 60^\circ$ $\alpha_2 = 30^\circ$	$a_1 = 0,7 t$ $a_2 = 0,7 t$ $b \le 2 \text{ mm}$ $m \ge 3 \text{ mm}$ $4 \text{ mm} \le t \le 10 \text{ mm}$		Application/ condition
	Fillet welded flange.	Loose flange.	Note
	3.1.2 and 3.1.1	2.11 and 1.9.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 5 (continued)

5.1.7	5.1.6	no.
		Figure
r = 7 mm $10^{\circ} \le \alpha \le 20^{\circ}$ $a \ge 0,7 t$ $h \ge 0,7 t$	r = 7 mm $h_1 \ge 0, 7 t$ $h_2 \ge 0, 7 t$ $45^{\circ} \le \alpha_1 \le 60^{\circ}$ $10^{\circ} \le \alpha_2 \le 20^{\circ}$	Application/ condition
		Note
		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 5 (continued)

5.1.9	5.1.8	no.
# # #		Figure
1 conventional butt weld	$a \ge 0,7 t$ $5 \text{ mm} \ge m = 0,5 t$ $b \ge 5 \text{ mm}$ $n \ge 5 \text{ mm}$ $\alpha = 15^{\circ}$	Application/ condition
For lower pressures and smaller pipe diameters or pipes in stainless steel with flange made of carbon steel.		Note
.3	1.4	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 — Jacketed vessels

	no.
	Figure
	Application/ condition
	Note
1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

It is recommended that the gap between the shell of the vessel and the jacket or blocking ring should not exceed 3 mm. A blocking ring should be machined to a circumferential length not more than 5 mm greater than that of the vessel. Wider gaps increase the tendency to spontaneous cracking during welding, particularly as the thickness of the parts increase.

	<i>a</i> ₁	
2	$45^{\circ} \le \alpha_1 \le 60^{\circ}$ $35^{\circ} \le \alpha_2 \le 60^{\circ}$	1 jacket 2 shell 2 mm $\leq b \leq 4$ mm
 if the shell plate is stressed in direction of its thickness, it shall be examined for laminations before welding the jacket. 	 in difficult situations, chamfering the blocking ring will help to avoid cracking; 	 As service conditions become more severe, change to full penetration weld;

Table 6 (continued)

6.1.3	6.1.2	no.
t_1 t_2	b b	Figure
$t_2 \le 15 \text{ mm}$ $45^\circ \le \alpha \le 60^\circ$ or as calculated 1 sealing run	a≥0,7 t b≤2 mm	Application/ condition
	see 6.1.1	Note
	4.1.3 and 1.5	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.1.6	6.1.5	6.1.4	no.
		b b	Figure
α = 45°	$3 \text{ mm} \ge a \ge 0,7 t$ $\alpha = 45^{\circ}$	2 mm ≤ b ≤ 4 mm 45° ≤ α ≤ 60°	Application/ condition
		see 6.1.1	Note
2.9.1 and 1.9.1	1.9.1	2.9.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.2. ₂	6.2.1		no.
			Figure
1 see Figure 5.1.1 for weld size and profile	a = 0,5 t b ≤ 2 mm	6.2 Blocking rings	Application/ condition
	Alternative ring to shell weld 4.1.3 detail permissible when t does not exceed 15 mm		Note
2.11	s 4.1.3		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.3.3	6.3.2	6.3.1		no.
	b	d m	6.3 Intermediat	Figure
1 circular ring with vent holes	$3 \text{ mm} \ge a \ge 0,7 t$ $45^{\circ} \le \alpha \le 60^{\circ}$ $b = 2 \text{ mm}$	d≥2 m	Intermediate connections between shell and jacket	Application/ condition
For use on pressure vessels, when there is no risk of corrosion.			ell and jacket	Note
3.1.2 and 3.1.1	4.1.3 and 1.9.1	2.8 and 1.9.1		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

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	3	3
	=	÷
	2	ž
	q	D
,	٤	7

6.3.4	no.
	Figure
$45^{\circ} \le \alpha \le 60^{\circ}$ Dimensions defined by construction.	Application/ condition
for b) and c) = For use on pressure vessels, when there is no risk of corrosion.	Note
3.1.2 and 3.1.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.4.3	6.4.2	6.4.1		no.
	α,			Figure
1 gap 2 mm to 3 mm 2 good access to the weld between the inner shell and branch is required. h ≥ m α = 45°	May be welded from the outside only. $\alpha_1 = 60^{\circ}$ $\alpha_2 = 45^{\circ}$	Inside shell accessible for welding. $\alpha = 45^{\circ}$	6.4 Branch connections	Application/ condition
These details are for use only when it is necessary for the jacket to extend up the branch.	It is necessary to ensure good access to the weld between inner shell and branch. Not applicable for alternating bend stress, e.g. effected by temperature difference between inner vessel and outer shell of the vessel.	Not applicable for alternating bend stress, e.g. effected by temperature difference between inner vessel and outer shell of the vessel.		Note
1.9.1	1.9.1 and 1.3	1.9.1		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.4.6	6.4.5	6.4.4	no.
#	#		Figure
f≥r	<i>f</i> ≥ 20 mm	If the branch to shell weld has to be welded on both sides, the branch jacket shall be made of two halves. Note welding sequence: $1 - 11 - 111 - 111$. $\alpha = 45^{\circ}$	Application/ condition
		see 6.4.3	Note
1.9.1	4.1.3	1.3 and 1.9.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.4.9	6.4.8	6.4.7	no.
#		#	Figure
1 conventional butt weld	$10^{\circ} \le \alpha \le 20^{\circ}$ $b = 5 \text{ mm}$ $n > 2 \text{ mm}$		Application/ condition
	For use on pressure vessels, when there is no risk of corrosion.	These branch connections are preferably used in the heads of jacketed vessels. Some of the details may also be applied in other region of the jacketed vessels. Not applicable for alternating bend stress, e.g. effected by temperature difference between inner vessel and outer shell of the vessel.	Note
2.5.2 or 2.6 and 1.5		4.1.3 and 1.9.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

6.5.4	6.5.3	6.5.2	6.5.1	Preformed		no.
	#####	a l		Preformed elements welded to shell. Good accessibility is required for welding.	6.5	Figure
3 mm ≥ a≥t α = 45° c ≤ 1 mm t≥ 2,6 mm	t≤ 2,6 mm a≥t	$\alpha_1 = 45^\circ$ $\alpha_2 = 60^\circ$ $2 \text{ mm} \le b \le 3 \text{ mm}$	1 shell α = 45°	ed for welding.	Alternatives to full jackets	Application/ condition
Full penetration.				C	n	Note
		1.9.1	1.9.1			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 6 (continued)

no.	Figure	Application/ condition	Note	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998
6.5.5	a a a a a a a a a a a a a a a a a a a	t > 2,6 mm $2 \text{ mm} \le b \le 4 \text{ mm}$ $\alpha = 45^{\circ}$ $a \ge t$	Full penetration.	1.9.1
		6.6 Staybolt connections		
To have the	To have the possibility of detecting cracks in the bolt.			8
0.0.2		1 alternative weld preparation to 2	Staybolt normal arrangement.	1.9.1 and 1.9

Table 7 — Tube to tube plate connection

Tubes are w	no.	
Tubes are welded to tube plates by several processes like manual metal-arc welding and mainly by	Figure	
al metal-arc welding and maj	Application/ condition	
nly by partly and fully mechanized TIG-welding	Note	
「IG-welding	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998	

It is advisable to examine the tube plate for laminations before machining.

Tubes shall closely fit their holes.

Care should be taken to ensure that the tube ends and tube plate holes are clean before welding.

The holes in the tube plates shall be deburred.

If two runs are welded, the second run shall fully overlap the first one.

	7.1 1	7.1 Tube to tube plate connection	on	
7.1.1	# #	<i>t</i> ≤ 2,6 mm		
		0 mm ≤ x ≤ 2 mm		
7.1.2	##	t > 2,6 mm		3.1.1
	**************************************	x ≥ 6 mm		

Table 7 (continued)

no.	Figure	Application/ condition	Note	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998
7.1.3	h + x	t > 2,6 mm $t \le h \le 1,5 t$		
		x = h - 1 mm		
		r=t		
	†			
7.1.4	- + +	h≈t		
	h x	x = h - 1 mm		
		<i>t</i> ≥ 5 mm		
		$45^{\circ} \le \alpha \le 60^{\circ}$		
	# #			
7.1.5	a d	W = t		
	+	h≈t		
	m h	$1,5 \text{ mm} \le m \le 2 t$		
	- -	t≥5 mm		
		α = 30°		
	+			

Table 7 (continued)

7.1.7	7.1.6	no.
		Figure
w = t x = 0.5 w $0.5 \text{ mm} \le m \le 2 t$ h = 0.5 t	w = t 1,5 mm $\le m \le 2t$ for $t < 5$ mm	Application/ condition
Internal bore welding. Only for fully mechanized TIGwelding.		Note
	1.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

7.1.9 7.1.8 no. Figure h = 0.5 tW = t1≥1,5 t x = 0.5 W $1,5 \text{ mm} \le m \le 2 t$ Application/ condition see 7.1.7 Note Reference to EN ISO 9692-1:2003 and EN ISO 9692-2:1998

Table 7 (continued)

Table 8 — Flate end or tube plate to shell connections

8.1.3	8.1.2	8.1.1	When using		no.
Q.			When using details like 8.1.1, 8.1.2, 8.1.3, 8.1.7, 8.1.8, 8.1.9 special care shall be taken to ensure that the end plate is not laminated.	8.1 Flaten	Figure
a≥5 mm α=45°		<i>a</i> ≥ 0,7 <i>t</i>	cial care shall be taken to en	Flat end or tube plate to shell connections	Application/ condition
Typical connections used in the construction of waste heat boilers, economizers and fireboxes.		Accessible for welding on both sides of the shell.	sure that the end plate is not laminat	nections	Note
1.9.1	2.9.1 or 2.11	4.1.3	ted.		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 8 (continued)

8.1.4	no.
	Figure
$t_2 \le 15 \text{ mm}$ $t = t_1$ $45^\circ \le \alpha \le 60^\circ$	Application/ condition
For thin tube plates and for thick 3.1.1 flanges.	Note
3.1.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 8 (continued)

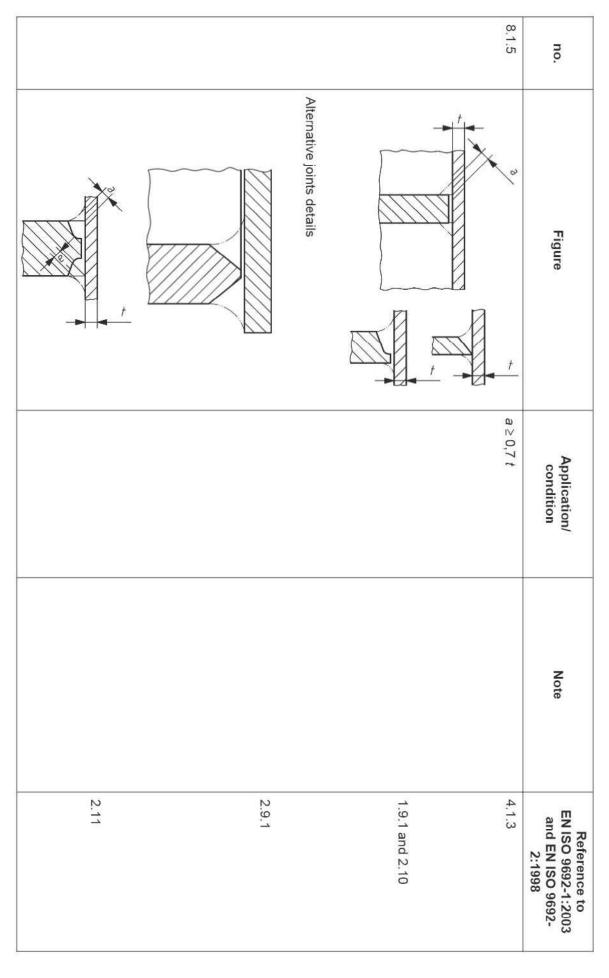


Table 8 (continued)

8.1.7	8.1.6	no.
	*	Figure
$n \ge 2$ mm Greater values of α are to be related to lower values of b and vice versa, e.g.: $\alpha = 10^{\circ}$ and $b = 15$ mm or $\alpha = 40^{\circ}$ and $b = 5$ mm	a ≥ 0,7 t 1 Instead of a cylindrical extension and a transition weld, the protruding part may be machined off.	Application/ condition
Permissible only for low static loading and when there is no risk of corrosion.		Note
1.4	2.10	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 8 (continued)

8.1.9	8.1.8	no.
# "		Figure
n≥3 mm	$a \approx 3$ mm Greater values of α are to be related to lower values of b and vice versa, e.g.: $\alpha = 10^{\circ}$ and $b = 15$ mm or $\alpha = 40^{\circ}$ and $b = 5$ mm $n \ge 2$ mm	Application/ condition
The shape of the groove in the flate end shall be designed depending on the service conditions. Not accepted for collectors in power plans.	See 8.1.7	Note
1.5	3.1.1	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

EN 1708-1:2010 (E)

Table 8 (continued)

8.1.11 8.1.10 no. Figure d ď ib ▼ but also $r_{\rm ik} \ge 5$ mm $r_{\rm ik} \ge 0.3 e_{\rm s}$ but also $r_{ik} \ge 5 \text{ mm}$ $r_{\rm lk} \ge 0.3 e_{\rm h}$ d_i ≤ 600 mm Application/ condition Note Reference to EN ISO 9692-1:2003 and EN ISO 9692-2:1998

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Table 8 (continued)

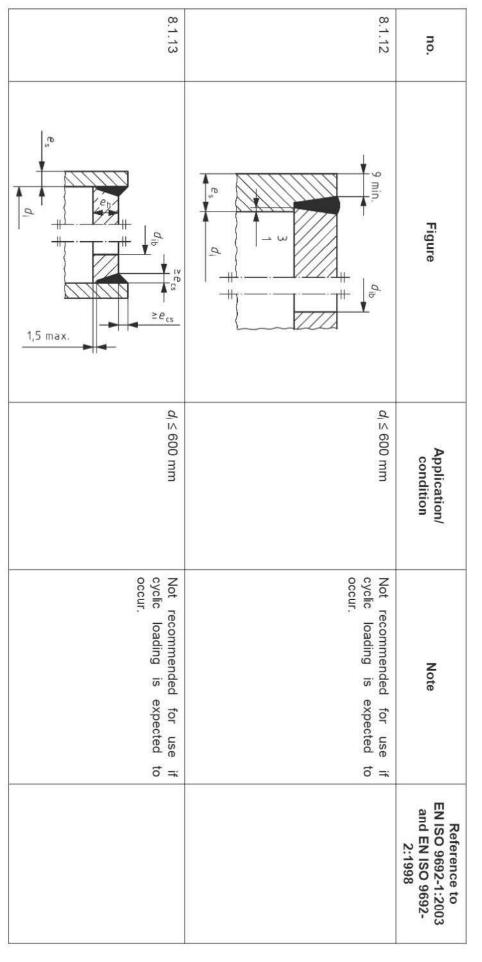


Table 9 — Internal diaphragms and separators

stationary 9.1.1	Figure only, suitable for differential pressure	Application/ condition 9.1 Internal diaphragms and separators Only of co	Note Note for use when there is no risk for use when there is no risk prosion.	Reference to EN ISO 9692-1:2003 and EN ISO 9692-2:1998 3.1.2 1.5 and 3.1.2
9.1.2	t ₂	$a \ge 0.7 t_3$ 25 mm $\ge n \ge 2 t_3$ 10 mm $\ge b \le 0.5 t_1$	Only for use when there is no risk of corrosion.	1.5 and 3.1.2
9.1.3			Conventional butt welds.	2.5.1 and 2.2

Table 10 — Supports and non-pressure parts

	no.
	Figure
	Application/ condition
	Note
2:1998	Reference to EN ISO 9692-1:2003 and EN ISO 9692-

influencing the quality of the pressure loaded parts. This applies in particular with respect to high yield-strengths materials. Influence of non-pressure parts. The welding consumables, the material and design of the non-pressure parts shall be such as to avoid unfavourable

concentrations Doubling plates. Doubling plates shall be used when attachment of non-pressure parts directly to the shell would cause unacceptable stress

Slots. In the case of slots, it shall be wide enough to allow a continuous fillet weld

Welding after final post-weld heat treatment. Welding of vessels, which have already been heat treated, is not permitted

Lifting facilities. Lifting facilities shall be made of the material which will avoid brittle fracture in low ambient temperatures

Vent holes. Where doubling plates are fitted before stress relief one or more vent holes shall be drilled in the plate.

Corner radii. Corners of doubling plate to be radiused to not less than three times thickness.

10.1.1 10.1 Supports for vessels be necessary. Vertical intermediate plate could 1.9.1

Table 10 (continued)

10.1.3	no.
Stiffener plates with or without mousehole	Figure
$a_1 = 0,5 t_2$ $a_2 \ge 0,5 t_3$ for $t_1 \le 15$ mm, $t_2 = t_1$ for $t_1 > 15$ mm, $t_2 < t_1$ $f \ge 10$ mm	Application/ condition
If the saddle is to be welded on the shell the following conditions shall apply: for $t_1 \le 15$ mm, $t_2 = t_1$ for $t_1 > 15$ mm, $t_2 < t_1$ a $\le 0,7$ t ₁ The weld shall be continued around the connecting part with $r \ge 30$ mm.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 10 (continued)

10.1.4	no.
	Figure
a > 4 mm	Application/ condition
For small vertical vessels.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 10 (continued)

	10.2.1		no.
X N N N N N N N N N N N N N N N N N N N		10.2 Sup	Figure
$m = 20 \text{ mm}$ $t_1 \le t_2 \le 1,5 t_1$ $a_1, a_2 = a$ $t_1, t_2 = t$ $a \le 0,7 t_{min}$	r≥ 10 mm	10.2 Supports for jacketed vertical vessels	Application/ condition
One vent hole required in the doubling plate.	All welds are circumferential.	vessels	Note
			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 10 (continued)

10.3.1		no.
$\frac{1}{2}$		Figure
$a_1, a_2 = a$ $t_1, t_2, t_3 = t$ $a \le 0, 7 t_{min}$ $t_1 \le t_2 \le 1, 5 t_1$ 1 vent hole	10.3 Non-pressure parts	Application/ condition
Lifting lug for heavy loads.		Note
		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 10 (continued)

10.3.2	no.
	Figure
a_1 , $a_2 = a$ t_1 , t_2 , $t_3 = t$ $a \le 0,7$ t_{min} $t_1 \le t_2 \le 1,5$ t_1 $r \ge 10$ mm 1 vent hole	Application/ condition
	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

10.3.4	10.3.3	no.
		Figure
1 vent hole	a_1 , $a_2 = a$ t_1 , t_2 , $t_3 = t$ $a \le 0,7$ t_{min} $a_3 = 0,5$ t_1 $t_3 \le t_2 \le 1,5$ t_3 1 vent hole	Application/ condition
		Note
		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

11.1.1 no. Figure t ≤ 8 mm 11.1 Joggle point Application/ condition and service conditions. Only for use when there is no risk of corrosion, fatigues, vibration Note Reference to EN ISO 9692-1:2003 and EN ISO 9692-2:1998

Table 11 — Special shell to head end connections

Table 12 — Weld ring seal

12.1.2	12.1.1		no.
			Figure
$\alpha = 120^{\circ}$ $\beta = 20^{\circ}$ $t = 4 \text{ mm}$	$\alpha = 120^{\circ}$ $m = 5 \text{ mm}$ $n = 6,5 \text{ mm}$ $q = 15 \text{ mm}$ $t = 3,5 \text{ mm}$	12.1 Weld ring seal	Application/ condition
Buttering on the flange side may be necessary at the location where the fillet weld is to be made.	Buttering on the flange side may be necessary at the location where the fillet weld is to be made.		Note
			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 12 (continued)

12.1.3	no.
	Figure
$\alpha = 120^{\circ}$ $m = 5 \text{ mm}$ $q = 15 \text{ mm}$	Application/ condition
Buttering on the flange side may be necessary at the location where the fillet weld is to be made.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 13 — Pipe details

no.
Figure
Application/ condition
Note
Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Pipe butt joints.

Butt joints incorporating backing rings.

Permanent backing rings may be used for butt welding of pipes that do not carry corrosive fluids provided proper precautions are taken to ensure freedom from non-metallic inclusions and root cracks. They are not recommended in case of fatigue load.

These precautions include the following:

- The gap between the ring and the bores of both pipes shall be kept to a minimum and in no case should exceed 0,4 mm. This will require the pipe ends to be bore trimmed by machining for roundness, and fit.
- Particular attention should be paid to such factors as the root gap, the root face, the thickness of the backing ring and the welding procedure.
- The backing ring should not cause the joint to be restrained whilst contracting.
- The misalignment is contained in EN ISO 5817.
- 1 In the case of corrosion, fatigue or creep the use of backing rings is generally not recommended

Table 13 (continued)

	no.
	Figure
13.1 Socket joints	Application/ condition
	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Socket joints are permitted on pipes with external diameter lower than 80 mm, with the dimensions indicated on 13.1.1.

Socket joints are anyway excluded:

- for steel pipes special applications;
- in parts exposed to fumes or to flame radiation;
- in those cases in which the service conditions, with particular regard to corrosion and fatigue stress, compromise the socket joint safety, in the opinion of the manufacturer.

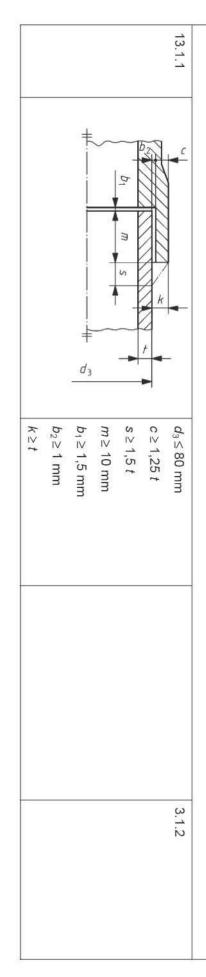


Table 13 (continued)

13.2.2	13.2.1	In case of	no.
A A A A A A A A A A A A A A A A A A A		13.2 Special branch connections In case of corrosion, fatigue, vibration service conditions the use of backing rings is generally not	Figure
b A	B - B	13.2 conditions the use	
The maximum angle β of slope should be 30° from the normal. Where the angle is greater than 30° special consideration shall be given to joint design and fabrication. $\alpha \ge 45^{\circ}$ 2 mm $\le b \le 4$ mm 1 mm $\le c \le 3$ mm	2 mm $\le b \le 4$ mm 1 mm $\le c \le 3$ mm $45^{\circ} \le \alpha \le 60^{\circ}$	Special branch connections of backing rings is generally no	Application/ condition
Set-on sloping unequal branch with bevel.	Equal set-on branch with bevel (for unequal branch connections see Table 2). 1 When the hole in the main pipe is thermal cut the ledge illustrated should be removed by grinding if required. Alternatively, if the hole in the main pipe is prepared by machining this ledge will not be obtained.	not recommended. For normal cases see Table 2.	Note
		see Table 2.	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 13 (continued)

13.2.3	no.
X B B B B B B	Figure
1 3 mm ledge obtained when thermal cutting hole in main pipe, see condition in 13.2.1. 2 Alternative profile. Main pipe ground locally to improve access. 2 mm $\leq b \leq 4$ mm 1 mm $\leq c \leq 3$ mm $\alpha_1 = 45^\circ$ $\alpha_2 \geq 35^\circ$ $\beta \leq 30^\circ$	Application/ condition
Set-on sloping equal branch with bevel.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 13 (continued)

13.2.5	13.2.4	no.
A-A	X X B B B B B B B B B B B B B B B B B B	Figure
The maximum angle β of slope shall be 30° from the normal. Where the angle is greater than 30° special consideration shall be given to joint design and fabrication. $\alpha \ge 45^{\circ}$ 2 mm $\le b \le 4$ mm 1 mm $\le c \le 3$ mm	$\alpha_1 \ge 60^\circ$ $\alpha_2 \ge 45^\circ$ $2 \text{ mm} \le b \le 4 \text{ mm}$ $1 \text{ mm} \le c \le 3 \text{ mm}$	Application/ condition
Unequal set-in sloping branch.	Equal set-in branch.	Note
		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 13 (continued)

	13.2.6	no.
	B-B	Figure
1 mm ≤ c ≤ 3 mm $ \alpha_1 \ge 45^{\circ} $ $ \alpha_2 \ge 60^{\circ} $ $ \alpha_3 \ge 45^{\circ} $ $ \alpha_4 \ge 35^{\circ} $ $ \beta \le 30^{\circ} $	$2 \text{ mm} \le b \le 4 \text{ mm}$	Application/ condition
	see 13.2.5	Note
		Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 14 — Block flanges

14.1.3	14.1.2	14.1.1		no.
h ZZ				Figure
2 mm $\le b \le 4$ mm $h = 0.5 t_2$ $z \approx 0.3 t_2$ $45^{\circ} \le \alpha \le 60^{\circ}$	4 mm $\leq t_2 \leq$ 30 mm without additional stress $a = 0,7 t_2$ $h \geq t_2$ $45^\circ \leq \alpha \leq 60^\circ$	4 mm $\le t_2 \le$ 10 mm without additional stress $a = 0,7 \ t_2$ $h \ge t_2$	14.1 Inserted block flanges	Application/ condition
		For spherical, shell and plane slab		Note
				Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 14 (continued)

14.1.6	14.1.5	14.1.4	no.
b 000 100 100 100 100 100 100 100 100 10			Figure
2 mm $\leq b \leq 4$ mm $z \approx 0,3 t_2$ $45^{\circ} \leq \alpha \leq 60^{\circ}$	$D_{ m W}$ = D + (1,5 to 2) $ imes$ $t_{ m 2min}$ 1 conventional butt weld	$2 \text{ mm} \le b \le 4 \text{ mm}$ $z \approx 0,3 t_2$ 1 Flange shall be ground flush inside (e.g. discharging drain) $45^{\circ} \le \alpha \le 60^{\circ}$	Application/ condition
For spherical, shell and plane slab during one-sided load.	Universal for spherical and plane slab without limiting of wall thickness t_2 , particularly for additional stress	Flange shall be flush inside (e.g. discharging spout)	Note
			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 14 (continued)

14.2.2	14.2.1		no.
h ₁ h ₂	h		Figure
$h_2 \le 3$ mm, otherwise fit $a = 0.5$ $t_2 \ge 5$ mm $z = 0.7$ t_2 , whereas t_2 shall be measured completely $e = 0.5$ t_2 , at least 10 mm	$a = 0.5 t_2 \ge 5 \text{ mm}$ $z = 0.7 t_2$, whereas t_2 shall be measured completely	14.2 Added block flanges	Application/ condition
For spherical and shell, if $h_1 \le 15$ mm $t_2 \le 30$ mm Tapped hole carry out as tapped thorough hole or tapped blind hole.	For spherical, shell and plane slab, if $h \le 3$ mm $t_2 \le 30$ mm Tapped hole carry out as tapped thorough hole or tapped blind hole. For $h \le 1$ mm (e.g. inspection glasses) is $a = 0.5$ $t_2 \ge 3$ mm.		Note
			Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998

Table 14 (continued)

14.2.3	no.
	Figure
$h_2 \le 3$ mm, otherwise fit $t_1 \approx t_2$ $a = 0,5$ $t_2 \ge 5$ mm $a_1 = 0,5$ $t_2 \le 6$ mm $z = 0,7$ t_2 , whereas t_2 shall be measured completely	Application/ condition
For spherical and shell, if $h_1 \ge 15$ mm $t_2 \le 30$ mm Tapped hole carry out as tapped thorough hole or tapped blind hole.	Note
	Reference to EN ISO 9692-1:2003 and EN ISO 9692- 2:1998